

On Dynamic Pressure to Side Wall of a Box Filled Sand

by

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ABSTRACT

Plain strain state equilibrium is taken for the above subject and analysis will be carried on by means of finite Fourier transforms.

1. General Solution

Under the stationary vibration $\sin \gamma t$, we can write the displacement Components in the x, y directions as $U \sin \gamma t$, and the component of stresses as $\sigma_x \sin \gamma t$, $\sigma_y \sin \gamma t$, $\tau_{xy} \sin \gamma t$. (Fig. 1)

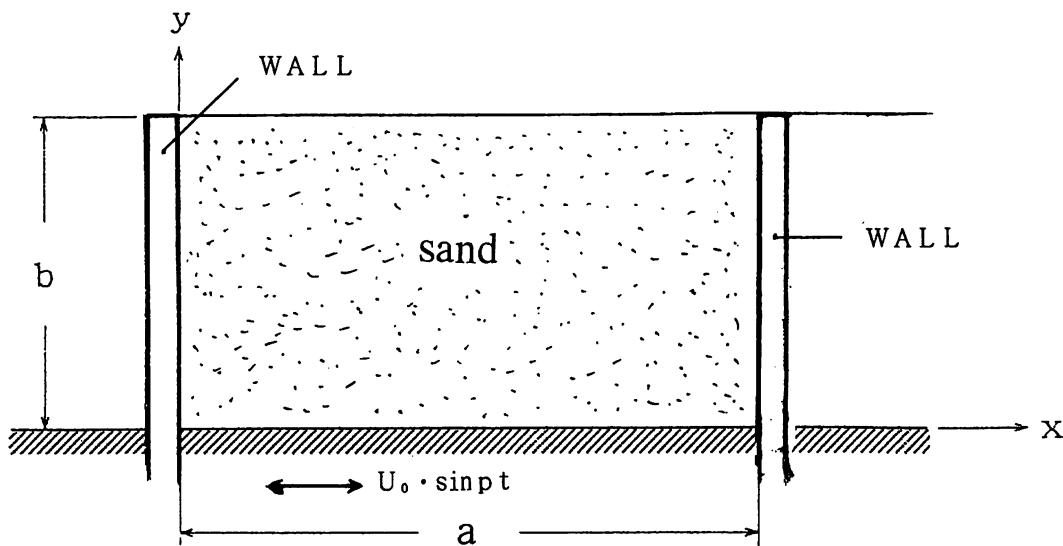


Fig. 1 Model of Analysis

So doing, the equilibrium of forces are expressed

$$\text{by } \frac{\partial \sigma_x}{\partial x} + \frac{\partial \tau_{xy}}{\partial y} + \rho \ddot{U} = -\rho \ddot{U}_0 \quad (1)$$

$$\frac{\partial \sigma_y}{\partial y} + \frac{\partial \tau_{xy}}{\partial x} + \rho \ddot{V} = -g \rho \quad (2)$$

in which U is the displacement in x direction

V is the displacement in y direction with ρq

Hooke's Law is expressed by

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$$\rho \begin{vmatrix} c_1^2 \frac{\partial}{\partial x} & (c_1^2 - 2c_2^2) \frac{\partial}{\partial y} \\ (c_1^2 - 2c_2^2) \frac{\partial}{\partial x} & c_2^2 \frac{\partial}{\partial y} \\ c_2^2 \frac{\partial}{\partial y} & c_2^2 \frac{\partial}{\partial x} \end{vmatrix} = \begin{Bmatrix} U \\ V \end{Bmatrix} = \begin{Bmatrix} \sigma_x \\ \sigma_y \\ \tau_{xy} \end{Bmatrix} \quad (3)$$

where $(2G + \lambda) = C_1^2 \rho$ $G = C_2^2 \rho$
 ρ = density of Sand $C_1 = C_2$ = bulk and distortion velocities

Multiplying L_1, L_2 with (1) and (2) and integrating by parts, We have

$$\int_0^a \left[\frac{\sigma_x}{\rho} L_1 \right] dy - C_1^2 \int_0^a U \frac{\partial L_1}{\partial x} dy - (C_1^2 - 2C_2^2) \int_0^a V \frac{\partial L_1}{\partial x} dy \\ + \int_0^a \left[\frac{\tau_{xy}}{\rho} L_1 \right] dx - C_2^2 \int_0^a U \frac{\partial L_1}{\partial y} dx - C_2^2 \int_0^a V \frac{\partial L_1}{\partial y} dx \\ + \int_A U (C_1^2 \frac{\partial^2 L_1}{\partial x^2} + C_2^2 \frac{\partial^2 L_1}{\partial y^2} + \gamma^2) dA + \int_A V (C_1^2 - C_2^2) \frac{\partial^2 L_1}{\partial x \partial y} dA = - \int_A U_0 L_1 dA \quad (4)$$

$$\int_0^a \left[\frac{\sigma_y}{\rho} L_2 \right] dx - C_1^2 \int_0^a V \frac{\partial L_2}{\partial y} dx \\ - (C_1^2 - 2C_2^2) \int_0^a U \frac{\partial L_2}{\partial y} dy + \int_0^a \left[\frac{\tau_{xy}}{\rho} L_2 \right] dy - C_2^2 \int_0^a V \frac{\partial L_2}{\partial x} dy \\ - C_2^2 \int_0^a U \frac{\partial L_2}{\partial x} dx + \int_A V (C_1^2 \frac{\partial^2 L_2}{\partial y^2} + C_2^2 \frac{\partial^2 L_2}{\partial x^2} + \gamma^2) dA \\ + \int_A U (C_1^2 - C_2^2) \frac{\partial^2 L_2}{\partial x \partial y} dA = 0 \quad (5)$$

Let $L_1 = \sin Mx \cdot \sin Ny$

where $M = \frac{m\pi}{a}, N = \frac{n\pi}{b}; m, n = 1, 2, 3, \dots$

$$- C_1^2 \{ S_n [U_{ay}] (-1)^m - S_n [U_{0y}] \} M - C_2^2 \{ S_m [U_{xb}] (-1)^n - S_m [U_{x0}] \} N \\ - S_m S_n [U] \cdot (C_1^2 M^2 + C_2^2 N^2 - \gamma^2) + C_m C_n [V] \cdot (C_1^2 - C_2^2) MN \\ = - \gamma^2 S_m S_n [U_0] \quad (6)$$

Let $L_2 = \cos Mx \cdot \cos Ny$

$$\frac{1}{\rho} \{ C_m [(\sigma_y)_{y=b}] (-1)^n - C_m [(\sigma_y)_{y=0}] \} + (C_1^2 - 2C_2^2) N \{ S_n [U_{ay}] (-1)^m - S_n [U_{0y}] \} \\ + \frac{1}{\rho} \{ C_n [(\tau_{xy})_{y=a}] (-1)^m - C_n [(\tau_{xy})_{x=0}] \} + C_2^2 M \{ S_m [U_{xb}] (-1)^n - S_m [U_{x0}] \} \\ - C_m C_n [V] (C_1^2 N^2 + C_2^2 M^2 - \gamma^2) + S_m S_n [U] (C_1^2 - C_2^2) MN = 0 \quad (7)$$

The case of $m = 0, n \neq 0$, (7) is expressed as

$$\frac{1}{\rho} \{ C_0 [(\sigma_y)_{y=b}] (-1)^n - C_0 [(\sigma_y)_{y=0}] \} + (C_1^2 - 2C_2^2) N \{ S_n [U_{ay}] - S_n [U_{0y}] \} \\ - \frac{1}{\rho} C_n [(\tau_{xy})_{x=0}] - C_n [(\tau_{xy})_{x=0}] - C_0 C_n [V] (C_1^2 N^2 - \gamma^2) = 0 \quad (8)$$

The case of $m \neq 0, n = 0$, (7) is also expressed as

$$\begin{aligned} & \frac{1}{\rho} \{ C_m [(\sigma_y)_{y=b}] - C_m [(\sigma_y)_{y=0}] \} + \frac{1}{\rho} \{ C_0 [(\tau_{xy})_{x=0}] - C_0 [(\tau_{xy})_{x=0}] \} \\ & + C_2^2 M \{ S_m [U_{xb}] - S_m [U_{x0}] \} - C_m C_0 [V] (C_2^2 M^2 - \gamma^2) = 0 \end{aligned} \quad (9)$$

Then, the case of $m = 0, n = 0$, (7) is shown as following

$$\begin{aligned} & \frac{1}{\rho} \{ C_0 [(\sigma_y)_{y=b}] - C_0 [(\sigma_y)_{y=0}] \} + \frac{1}{\rho} \{ C_0 [(\tau_{xy})_{x=a}] - C_0 [(\tau_{xy})_{x=0}] \} \\ & + C_0 C_0 [V] \gamma^2 = 0 \end{aligned} \quad (10)$$

For convenience sake, putting

$$S_m S_n [U] = U_{mn}, \quad C_m C_n [V] = V_{mn},$$

then we have

$$\begin{aligned} & \left| \begin{array}{cc} C_1^2 M^2 + C_2^2 N^2 - \gamma^2 & -[C_1^2 - C_2^2] MN \\ -(C_1^2 - C_2^2) MN & C_1^2 N^2 + C_2^2 M^2 - \gamma^2 \end{array} \right| \left\{ \begin{array}{c} U_{mn} \\ V_{mn} \end{array} \right\} \\ & = \left\{ \begin{array}{c} \gamma^2 S_m S_n [U_0] - N(-1)^n C_2^2 S_m [U_{xb}] \\ -\frac{1}{\rho} C_m [(\sigma_y)_{y=0}] + M(-1)^n C_2^2 S_m [U_{xb}] \\ + \frac{1}{\rho} \{ C_n [(\tau_{xy})_{x=a}] (-1)^m - C_n [(\tau_{xy})_{x=0}] \} \end{array} \right\} \end{aligned} \quad (11)$$

By putting again in the above

$$\begin{aligned} \frac{C_2^2}{C_1^2} &= \kappa, \quad \frac{\gamma^2}{C_1^2} = p^2, \quad F_{mn} = p^2 S_m S_n [U_0] = U_0 p^2 (1 - (-1)^m)(1 - (-1)^n) MN \\ S_m [U_{xb}] &= A_m, \quad \frac{1}{\rho} C_m [(\sigma_y)_{y=0}] = B_m \end{aligned}$$

And, the boundary condition are so given as to come

$$\begin{aligned} \text{for } x = 0, a, \quad u = 0, \quad \tau_{xy} = 0; \text{ and } y = 0, \quad \sigma_y = 0, \quad \tau_{xy} = 0; \text{ and} \\ y = b, \quad v = 0, \quad u = 0. \end{aligned}$$

$$\left| \begin{array}{cc} M^2 + \kappa N^2 - p^2 & -(1-\kappa) MN \\ -(1-\kappa) MN & \kappa M^2 + N^2 - p^2 \end{array} \right| \left\{ \begin{array}{c} U_{mn} \\ V_{mn} \end{array} \right\} = \left\{ \begin{array}{c} F_{mn} - \kappa A_m (-1)^n N \\ -B_m + \kappa A_m (-1)^m M \end{array} \right\} \quad (12)$$

Then,

$$U_{mn} = [F_{mn} (\kappa M^2 + N^2 - p^2) + \kappa A_m (-1)^n N ((1-2\kappa) M^2 - N^2 + p^2) \\ - (1-\kappa) MNB_m] / \Omega_{mn} \quad (13)$$

$$V_{mn} = [F_{mn} (1-\kappa) MN + \kappa A_m M \{ M^2 - (1-2\kappa) N^2 - p^2 \} \\ - (M^2 + \kappa N^2 - p^2) B_m] / \Omega_{mn} \quad (14)$$

where

$$\Omega_{mn} = \kappa (M^2 + N^2 - p^2) (M^2 + N^2 - \frac{p^2}{\kappa}) = \kappa HH'$$

$$H = M^2 + N^2 - p^2$$

$$H' = M^2 + N^2 - \frac{p^2}{\kappa}$$

These result are summed up to be following solutions by the finite Fourier inversion formula.

$$U = \sum_m \frac{(1 - (-1)^m)}{2} \sin Mx \left[\frac{4U_0}{b} \frac{b}{m\pi} \left\{ (1 - Q_m(\eta)) \frac{p^2}{\beta_m^2} \right. \right. \\ \left. \left. + (Q'_m(\eta) - Q_m(\eta)) \right\} - \frac{2hA_m e \pi}{b^2 p^2} \frac{b}{\pi} \left\{ 2(me)^2 (R'_m(\eta) \right. \right. \\ \left. \left. - R_m(\eta)) - p^2 R'_m(\eta) \right\} + \frac{2B_m e}{bp^2} \frac{b}{\pi} (me)(R_m(1 - \eta) \right. \\ \left. - R'_m(1 - \eta)) \right] \quad (15)$$

$$V = \sum_m \frac{(1 - (-1)^m)}{2} \cos Mx \left[\frac{4U_0}{b} \frac{be}{\pi} \left(\frac{\phi'_m(\eta)}{\beta'_m} - \frac{\phi_m(\eta)}{\beta_m} \right) \right. \\ \left. + \frac{2hA_m e \pi}{b^2 p^2} \frac{b}{\pi} (me) \left\{ 2(\beta'_m \phi'_m(\eta) - \beta_m \phi_m(\eta)) + \frac{p'^2}{\beta'_m} \phi'_m(\eta) \right\} \right. \\ \left. - \frac{2B_m e}{bp^2} \frac{b}{\pi} \left\{ \frac{(me)^2}{\beta'_m} \phi'_m(1 - \eta) - \beta_m \phi_m(1 - \eta) \right\} \right] \quad (16)$$

where

$$Q_m(\eta) = \frac{ch(\beta_m \pi (\frac{1}{2} - \eta))}{ch(\beta_m \pi / 2)} \quad \left[= \frac{\cos(\beta_m \pi (\frac{1}{2} - \eta))}{\cos(\beta_m \pi / 2)} \right]$$

$$R_m(\eta) = \frac{sh(\beta_m \pi \eta)}{sh(\beta_m \pi)} \quad \left[= \frac{\sin(\beta_m \pi \eta)}{\sin(\beta_m \pi)} \right]$$

$$R_m(1 - \eta) = \frac{sh(\beta_m \pi (1 - \eta))}{sh(\beta_m \pi)} \quad \left[= \frac{\sin(\beta_m \pi (1 - \eta))}{\sin(\beta_m \pi)} \right]$$

$$\phi_m(\eta) = \frac{ch(\beta_m \pi \eta)}{sh(\beta_m \pi)} \quad \left[= \frac{\cos(\beta_m \pi \eta)}{\sin(\beta_m \pi)} \right]$$

$$\phi_m(1 - \eta) = \frac{ch(\beta_m \pi (1 - \eta))}{sh(\beta_m \pi)} \quad \left[= \frac{\cos(\beta_m \pi (1 - \eta))}{\sin(\beta_m \pi)} \right]$$

$$\psi_m(\eta) = \frac{sh(\beta_m \pi (\frac{1}{2} - \eta))}{ch(\beta_m \pi / 2)} \quad \left[= \frac{\sin(\beta_m \pi (\frac{1}{2} - \eta))}{\cos(\beta_m \pi / 2)} \right]$$

$$Q'_m(\eta) = \frac{ch(\beta'_m \pi (\frac{1}{2} - \eta))}{ch(\beta'_m \pi / 2)} \quad \left[= \frac{\cos(\beta'_m \pi (\frac{1}{2} - \eta))}{\cos(\beta'_m \pi / 2)} \right]$$

$$R'_m(\eta) = \frac{sh(\beta'_m \pi \eta)}{sh(\beta'_m \pi)} \quad \left[= \frac{\sin(\beta'_m \pi \eta)}{\sin(\beta'_m \pi)} \right]$$

$$R'_m(1 - \eta) = \frac{sh(\beta'_m \pi (1 - \eta))}{sh(\beta'_m \pi)} \quad \left[= \frac{\sin(\beta'_m \pi (1 - \eta))}{\sin(\beta'_m \pi)} \right]$$

$$\begin{aligned}\phi'_m(\eta) &= \frac{ch(\beta'_m \pi \eta)}{sh(\beta'_m \pi)} \quad \left[= \frac{\cos(\beta'_m \pi \eta)}{\sin(\beta'_m \pi)} \right] \\ \phi'_m(1-\eta) &= \frac{ch(\beta'_m \pi (1-\eta))}{sh(\beta'_m \pi)} \quad \left[= \frac{\cos(\beta'_m \pi (1-\eta))}{\sin(\beta'_m \pi)} \right] \\ \psi'_m(\eta) &= \frac{sh\left(\beta'_m \pi \left(\frac{1}{2} - \eta\right)\right)}{ch(\beta'_m \pi / 2)} \quad \left[= \frac{\sin\left(\beta'_m \pi \left(\frac{1}{2} - \eta\right)\right)}{\cos(\beta'_m \pi / 2)} \right]\end{aligned}$$

$$\beta_m^2 = (me)^2 - p^2 \quad M = \frac{m\pi}{a} \quad \left[\begin{array}{l} \text{cage of} \\ \text{imaginary} \end{array} \right]$$

$$\beta'^2 = (me)^2 - p'^2 \quad \eta = \frac{y}{b}$$

$$p'^2 = p^2/h \quad e = \frac{b}{a}$$

$$h = \frac{C_2^2}{C_1^2} = \frac{G}{2G + \lambda} = \frac{1-2\nu}{2(1-\nu)}$$

ν : poisson's ratio

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